The opportunities disclosed by Avio capabilities and Vega LV availability in the field of hypersonic vehicles technologies.

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600



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1st International Symposium: "Hypersonic flight: from 100.000 to 400.000 ft" Rome, Italy, 30 June-1 July 2014





Vega Launch System at a Glance

Vega is conceived to complement the European family of launchers and to target the small payload in low Earth







Vega LV at a Glance

Despite its relatively low lift off mass (137 ton) **Vega is the largest launch vehicle mostly based on solid propulsion** (solid stages assure as much as 95% of its DV). **Vega LV architecture is as simple as possible:** three monolithic CFRP solid propulsion stages, an upper storable liquid Vernier that contains most of the avionic equipment and the roll and attitude control system, a choice of CFRP Payload Adapter and a F2.6m Payload Fairing. Four Al alloy interstage structures complete the airframe.

Height [m]	30.162
Maximum diameter [m]	3.005
Fairing diameter [m]	2.600
Mass at Lift-off [kg]	136740
Reference mission performance [kg]	1451
Structural Ratio	10.2%





Vega LV at a Glance

- Avionics is based on a single chain GNC subsystem (less than 20 parts), including an Inertial Navigation System and four electromechanical actuators for control of the thrust vector of each stage, a modular single chain telemetry subsystem
- Apart the Inertial Navigation System no sensor is functional for the flight.
- A Safeguard Subsystem (fully redounded) perform the main safeguard functions.
- Well proven **pyrotechnics devices** allow for motor ignition, liquid engine and thrusters configuration, priming, and passivation, solid rocket motor neutralization, stages separation, payload fairing release and payloads separation.
- Elastic elements (springs or Marman clamps) generate the stages separation force, with the exception of the first to second stage where six **retro-rockets provide** the necessary ΔV .



LV is transonic 30s after lift-off, around 50s attains the maximum dynamic pressure, @3 min reaches 4Km/s, @6min passes 7.5Km/s. The mission continues up to 12000s, and allows the orbit injection of 6 independent payloads.

3

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The upper stage may be re-ignited up to 5 times, allowing orbital plane changes for different payloads.

REFERENCE TRAJECTORY

7

8

11 AVUM Deorbiting T = 4057 s Z = 721 km V = 7501 m/s

R = 25381 km

End of Mission

T = 4073 s Z = 721 km V = 7451 m/s R = 25483 km

10

12

10

0

11

12

P/L Separation T = 3772 s Z = 715 km V = 7508 m/s R = 23527 km

9

AVUM Cut-Off, Orbit Circularization T = 3632 s Z = 712 km V = 7512 m/s R = 22620 km

1	2	3	4	5	6	7	8
P80FW Ignition & Lift-Off	Stage 1 Separation	Z23 Burnout	Stage 2 Separation	Fairing Separation	Stage 3 Separation	Transfer Orbit Injection	AVUM 2nd Ignition
T (mission time) = 0 s	T = 113 s	T = 191 s	T = 202 s	T = 229 s	T = 357 s	T = 798 s	T = 3481 s
Z (altitude) = 0 km	Z = 51 km	Z = 101km	Z = 107 km	Z = 118 km	Z = 140 km	Z = 141 km	Z = 707 km
V (relative speed) = 0 m/s	V = 1772 m/s	V = 3965 m/s	V = 3953 m/s	V = 3991 m/s	V = 7570 m/s	V = 7992 m/s	V = 7356 m/s
R (downrange) = 0 km	R = 76 km	R = 291 km	R = 332 km	R = 437 km	R = 1570 km	R = 4517 km	R = 21659 km

VEGA

700 KM - PEO

VESPA Separation T = 6385 s z = 676 km V = 7650 m/s R = 37000 km	AVUM 4th Ignition PL2 T = 6794 s T = 7 z = 678 km z = 6 V = 7646 m/s V = R = 38700 f. v R = 4	Separation 7035 s 881 km 7597 m/s 45500 km	PL3 Separation T = 7740 z z = 680 km V = 7598 m/s R = 50000 km	AVUM 5 th Ignition T = 8500 s r = 670 km V = 7613 m/s R = 55000 km		2 4	r f	7	-	0
	5 6	i i	7/8	9	1/2	J 4	5 0	-	0	9
			0		- - ()8 (• •	aid- cir	ű, "	Q	12-
	0	V	2 ^{3 4} EGA VV02	Mission	Profile	5	67	8	9	
17		3 P/	'I were iniected	l into 2 differe	nt orbits.					
V		ath a	taga narfarma	d the direct re					4	
n Ø		the	Pacific Ocean	a the direct re	-entry into			A T I V R	VUM 3rd Ignition = 3840 s = 837 km = 7520 m/s = 20780 km	
						1	2		3	
1	P80FW Ignition & Lift-Off T (minsion time) = 0 s z (altitude) = 0 km V (relative speed) = 0 m/s R (downrange) = 0 km	Stage 1 Separation T = 116 s z = 65 km V = 1690 m/s R = 70 km	Stage 2 Separation T = 220 z z = 180 km V = 3690 m/z R = 313 km	Fairing Separation T = 240 s z = 197 km V = 3700 m/s R = 392 km	Stage 3 Separation T = 378 s z = 262 km V = 7591 m/s R = 1040 km	u Transfer Orbit Injectiou T = 668 z z = 292 km V = 7965 m/z R = 2700 km	AVUM 2nd I T = 3183 x z = 822 km V = 7393 m/y R = 16800 km	gaition P T T V R	L1 Separation = 3334 s = 825 km = 7533 m/s = 17650 km	



IXV and Pride mission takes full advantage of Vega capabilities.



Next Vega Missions: drive IXV on suborbital re-entry path





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PL mass = 1927 kg Target Parameters at AVUM 1 cut-off:

- Perigee Altitude = 73.810 km
- Apogee Altitude = 420.066 km
- Inclination = 5.429 deg

	Trajectory up to AVUM 1 Shu							
Event	Time [s] / H0	Phase Duration [s]						
Imu Start	-2.0							
Lift Off	0.3							
Pitch-Over	4.5	11.6						
Gravity Turn	16.1	11.0						
1 st Sep.	114.4							
Z23 Ign.	115.3							
2 nd Sep.	218.0	20.7						
Z9 Ign.	238.7	20.7						
Fairing release	244.0							
3 rd Sep.	379.8	00						
AVUM 1 Ign.	469.8	90						
AVUM1 Shut.	760.1							

	Trajectory: PL release and deorbiting									
Event	Time [s] / H0	Phase Duration [s]								
PL release	1060.1	805								
AVUM 3 Ign.	1865.1	605								
AVUM 3 Shut.	1877.7	4719.0								
AVUM 5 Ign.	6596.6	4710.9								
AVUM 5 Shut.	6642.5									

Less than **20min** from lift-off to P/L release



Next Vega Missions: drive IXV on suborbital re-entry path



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Vega flexibility enables both direct and indirect re-entry missions.

AVUM upper stage allows any sort of orbital

maneuvers and performs a reentry itself.



PRIDE: a feasible Vega mission

Vega enables missions like Pride, presenting an orbital

and a distinct reentry phase.

This mission might also demonstrate in-orbit servicing

concept.



TRAJECTORY EVEN	TS										DV	_BALANC	E	
STAGE/EVENT	TIME	_REL.SP.	ALT.	WEIGHT	MACH_	P.DYN	(T-D)/M	GAM.R.	ALPHA_	DVprop	_DVgrav_	DVaero_	DVd1s_	Dvinert_
1 DMU Start	-2.0	[m/s] 0.0	[km] 0.0	[kg] 138943.6	8.3	[Pa] 0.0	[#/s2] 0.00	96.0	6.8	0.0	0.0	[m/s] 0.0	0.0	0.0
1 Motor Start	0.0	0.0	0.0	138943.6	0.0	0.0	0.00	90.0	0.0	0.0	0.0	0.0	0.0	0.0
1 Lift-off	0.3	0.0	0.0	138891.6	0.0	0.0	9.85	90.0	0.0	0.0	0.0	0.0	0.0	0.0
1 Pitch-Over	4.2	28.3	0.1	135152.8	0.1	468.9	18.42	89.9	0.2	66.5	-1.1	0.0	-64.6	0.9
1 q*alpha max	11.4	103.0	0.5	127444.5	0.3	5952.1	21.18	79.8	3.6	(22390.6	P&**)			
1 GravityTurn	14.2	136.1	0.8	124398.0	9.4	10090.0	21.50	76.2	0.0	272.0	-16.9	-0.1	-205.4	49.7
1 Mach 1	31.0	332.1		10/641.8	1.0	40539.5	17.50	61.2	0.0					
1 (T-p) /H max	27.2	1617 7	24.4	00041.4	613	30127.0	20.14	32.0	0.0					
1 AT DOT	114.5	1951-5	20.1	20690.3	5.2	12012-2	28.31	51.1	8.8	2644.2	-390.5	-119.4	-405.9	1728.5
1 Separation	114.7	1750.6	50.2	50687.3	6.5	1637.8	0.69	21.1	0.0	2644.4	-391.1	-119.4	-405.9	1728.0
2 Coasting		2130.0	30.1	30007.3		2037.0	0.05		0.0	2044.4			403.3	2120.0
2 Motor Start	115.5	1747.7	50.7	42198.3	5.3	1532.5	-0.06	20.8	0.0	2644.4	-391.1	-119.4	-405.9	1725.7
2 (T-D)/M max	160.0	3017.8	78.3	25794.3	10.9	125.2	35.19	12.0	15.1					
2 AT Det.	193.5	3876.2	102.5	18325.4	13.8	2.5	1.28	11.4	10.3	4981.5	-546.1	-120.8	-437.6	3874.5
2 Separation	218.3	3838.7	119.4	18299.3	10.0	0.2	0.00	9.0	0.0	4985.4	-571.4	-120.8	-437.7	3841.3
3 Coasting														
3 Motor Start	230.6	3821.7	126.3	15531.2	8.2	0.1	0.00	7.8	1.7	4985.4	-571.4	-120.8	-437.7	3826.2
3 HS Jettison	236.0	3874.7	129.0	15217.2	8.0	0.1	13.35	7.3	9.1	5045.2	-577.3	-120.8	-437.8	3879.9
3 (T-D)/M max	335-5	6807.5	168.7	5110.3	10.5	0.0	42.93	3-5	4.2					
5 AT DEL.	348.3	7210.7	1/4.1	4383.2	10.9	0.0	1.2/	3.0	34.7	8494.1	-035.1	-120.8	-408.4	7222.4
5 Separation	3/3.3	7202.2	185.5	43/6.6	10.5	0.0	0.03	2.9	33.9	8498.3	-004.2	-120.8	-409.5	7214.6
A Motor Start	1485.0	7016.7	329.2	2001.1	8.2	0.0	0.00	-1-1	29.9	8498 3	-664.2	-120.8	-469.3	7040.1
4 cut-off	1822.6	7241.3	300.0	2723.4	8.7	0.0	0.90	0.0	60.3	8787.5	-629.9	-120.8	-570.4	7262.6
4 Coasting														
4 Mtr Restart	3022.6	7251.0	292.1	2723.4	8.8	0.0	0.00	-0.1	0.0	8787.5	-629.9	-120.8	-570.4	7271.8
4 cut-off	3154.7	7168.8	286.6	2618.6	8.7	0.0	0.93	-0.6	153.4	8908.6	-623.4	-120.8	-780.4	7189.2
4 Coasting														
4 P/L Sep.	3304.7	7185.3	273.4	2618.6	8.9	0.0	0.00	-0.8	0.1	8908.6	-623.4	-120.8	-780.4	7204.7
4 Coasting														
4 alpha mäx	4185.5	7363.8	131.6	918.6	14.7	0.2	0.00	-1.5	179.6					
4 Deorbiting	4264.7	7382.8	116.5	918.6	20.5	0.9	0.01	-1-5	179.6	8908.6	-623.4	-121.1	-780.4	7390.7
(T-D)/M max	4304.7	7283.7	108.9	886.9	23.7	2.8	2.78	-1.5	177.1	0017.0				7341 4
4 Cut-off	4304.7	7283.7	108.9	886.9	25.7	2.8	2.78	-1.5	177.1	9017.0	-614.2	-121.7	-997.3	7291.0
 coasting 	4330.7	7367.3	105.0	005 0	24.2		0.04			0017.0	614.0		007.3	7204 44
 Passivation 	4320.7	/20/.5	102.8	686.9	24.7	4.8	-0.04	-1-5	12.8	9017.0	-614.2	-122.1	-997.5	7294.40

Legenda: columns report time, relative velocity, geodetic altitude, mass, Mach number, dynamic pressure, non-gravitational acceleration, flight path angle, angle of attack, the UV gains (propulsive) and losses (for gravity, aerodynamics, and incidence), and the total inertial UV



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12





Integrating Vega and re-entry vehicle control systems will increase the mission range.



USV- FTB AT

Avio recently studied and presented to CIRA the integration of a re-entry vehicle Flight Test Bench to Vega E. The proposal is twofold:

- Scale-up the vehicle envelope by designing an airframe able to fly w/o Vega Fairing. To possibly integrate aerodynamic control of FTB AT Vega GNC during ascent phase. This allows to test more efficient aerodynamic configurations than IXV (i.e. winged body), yet preserving the correct leading edge bluntness to survive reentry.
- Accommodate a cluster of Theseus LOx-Methane Re-ignitable thrusters. The cluster assures both the main propulsive function at full throttle and fractional (i.e. 1/2, 1/4,1/8) and the Attitude Control Function.



The cluster, arranged in aerospike shape (i.e. adapted at different altitudes)would deliver it propulsive and attitude function both in orbit and along the atmospheric re-entry path.



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USV- FTB AT

Theseus LOx-CH4 thruster is a 200N class high specific impulse bipropellant thruster under development in Avio. It is able to operate in both steady state and pulsed mode, thanks to the specific design of injector head and ignition system.

It will initiate test campaign on July 2014 in Avio Fast-2 static firing test bench.



USV FTB AT

The re-entry vehicle will boost after the AVUM phase in order to reach the required orbit. From such orbit a second boost will allow de-orbiting and insertion in atmosphere. Two boosts during the atmospheric flight will allow a longer flight , and larger mission flexibility.

The Flight Test Bench will be also invaluable for characterizing in altitude advanced hypersonic propulsion systems, starting from its own a aerospike engine.





Avio

USV- FTB AT (3/3)

Combining the USV- FTB AT and VEGA E it is possible to:

- increase the USV total mass to 3000 Kg with a 700-800 Kg of propellants for orbital change and re-enter maneuvers. It this way it is possible to widen the mission spectrum and allows possibility to carry (inside the vehicle) small high altitude experiments
- Install the VEGA avionics inside the Payload adapter. In this way it will be possible to recover the VEGA Avionics lowering the Launch cost. A possible use of VEGA avionics to pilot USV can be also evaluated avoiding in this way a duplication (recurrent cost









Avio is currently discussing with Reaction Engine Ltd an involvement in the Synergistic Airbreathing Rocket cycle



Reaction Engine Ltd: SABRE cycle intent

SABRE cycle intent is to overcome the issues of supersonic combustion stability by recover subsonic conditions of air captured by the intake by cooling the fluid more than simply compressing the flow. The idea, originated in the 50ties, has faced several implementation issues, cause of the failure of several programs (i.e. LACE, RB545 ...). Central to the Sabre thermodynamic concept is a Joule Brighton closed cycle (working fluid is He).



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once passed Mach 5, it reverts, by closing the dynamic intake, to a "classical" LOx-LH2 fuel rich staged combustion cycle.

SABRE is an hybrid engine:

Reaction Engine Ltd: SABRE cycle in two words

At hypersonic conditions, air compressed by the dynamic intake is regeneratively precooled by liquid He, then it is compressed in a turbo compressor and finally it is injected (for the most part) into a rocket combustion chamber.



intake air and drives, through a turbine expansion, the air turbo compressor, heats liquid hydrogen and drives LH2 pump high pressure stage.



Although application of SABRE to re-usable orbiters or spaceplanes is not obvious, the precooling cycle concept is gaining maturity and increasing TRL. Critical to this purpose is the design and demonstration of the air/LHE heat exchanger, whose efficiency is the driver for the engine feasibility.

In the past Avio was involved with REL in phases of LAPCAT studies.

Avio is currently discussing with REL for a partnership to design and develop the

turbomachinery (few of them not trivial) for a SABRE demonstrator.





Avio is currently proposing a roadmap for application of simple RAMJET propulsion to several dual use cases.



INTRODUCTION

- AVIO has a self-financed activities in the field of hypersonic vehicles and ramjet propulsion. AVIO has already proposed, in cooperation with CIRA, a roadmap relevant to the carry-on of propulsion system studies and component technology acquisition applied to hypersonic flight vehicles
- The above mentioned roadmap is aimed to extend the national access-to-space capabilities (today already achieved with the VEGA Launch Vehicle), and to exploit the wide dual-use opportunities offered by a single development activity.
 - **Reference missions UAV-1**: a unmanned atmospheric cruise vehicle whose lift-off and acceleration to cruise conditions is assured by a Solid Rocket Booster, while range is achieved by a ramjet. The vehicle is thought to carry 1 ton of dual P/L: i.e. hypersonic testing hardware or ammunitions.
 - Access to Space UAV-3: this is a reusable carrier for airborne launcher vehicles to provide fast orbit deployment of small P/L. The carrier is conceived to lift-off and accelerate by a standard turbojet (i.e. at the end of its operational life), reach hypersonic conditions and altitude by a ramjet engine, deploy the launch vehicle and close the mission by landing.

